

Seminar: *University of Bologna, 3 May 2000*

Reactive Security Study of a Large Power System

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Support: *TransGrid*



Outline (Bologna)

- ◆ Introduction
- ◆ System and Modelling
- ◆ Computation of the Security Boundary
- ◆ Application to NSW Main Grid
- ◆ Impact of Load Modelling
- ◆ Coordinated Control Schemes
- ◆ Conclusions

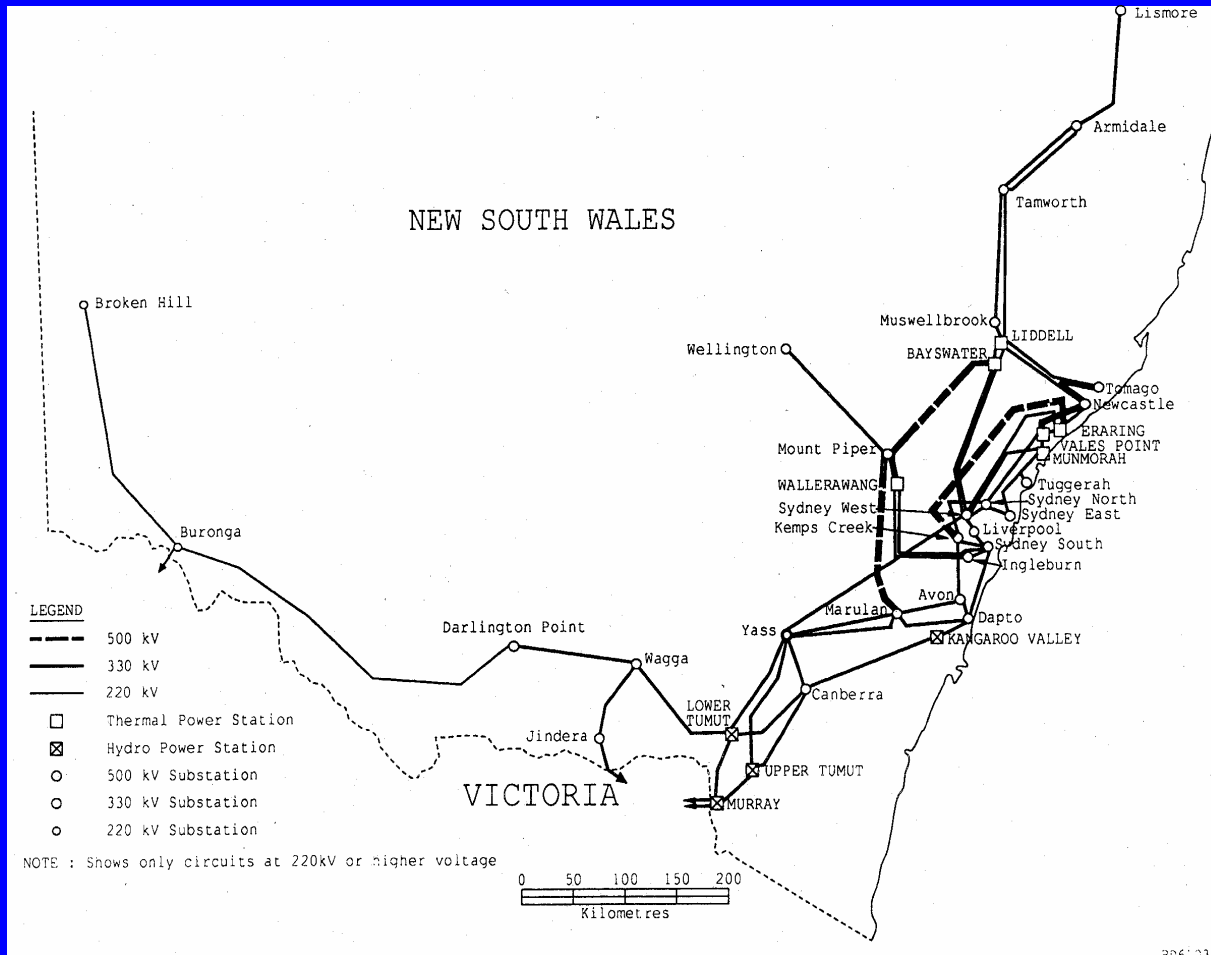


Introduction

- ◆ TransGrid is transmission company (TNSP) in National Electricity Market
- ◆ Voltage collapse determines limits (ATC)
- ◆ Contributing factors:
 - higher flows in NEM
 - load modelling
 - restriction on physical expansion
- ◆ Need stability margins more accurately



◆ NSW System



Key load centres

Bus 74 (Newc 330)

Bus 76 (Tomago330)

Bus 3229 (Newc 132)

Bus 3207 (SydW 132)

Bus 3283 (Syd E 132)

Bus 3286 (Syd S 132)

Bus 3172 (Dapto 132)

Bus 3101 (Canb 132)

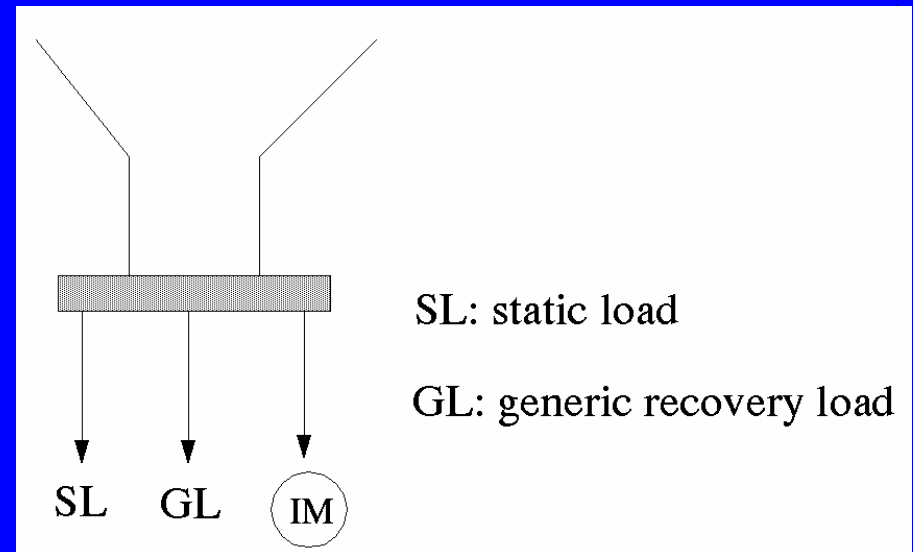


Composite Load Model

- ◆ Traditional PQ load model
- ◆ Generic dynamic model
- ◆ Aggregate induction motor model

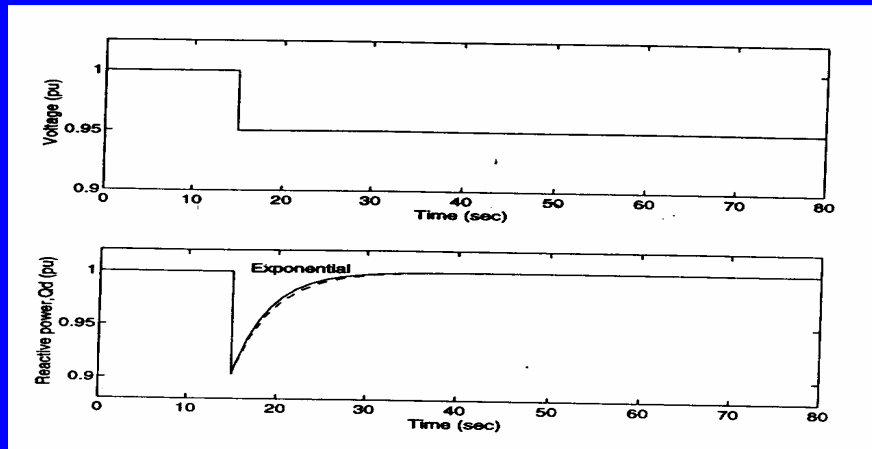
$$\text{Load} = w_1 SL + w_2 GL + w_3 IM$$

$$w_1 + w_2 + w_3 = 1$$



◆ Generic recovery load model

□ represent all down-stream OLTC and thermo-controlled loads



$$\dot{x}_p = P_s(V) - P_d$$

$$P_d = \frac{1}{T_p} x_p + P_t(V)$$

$$\dot{x}_q = Q_s(V) - Q_d$$

$$Q_d = \frac{1}{T_q} x_q + Q_t(V)$$

Step response of the load model

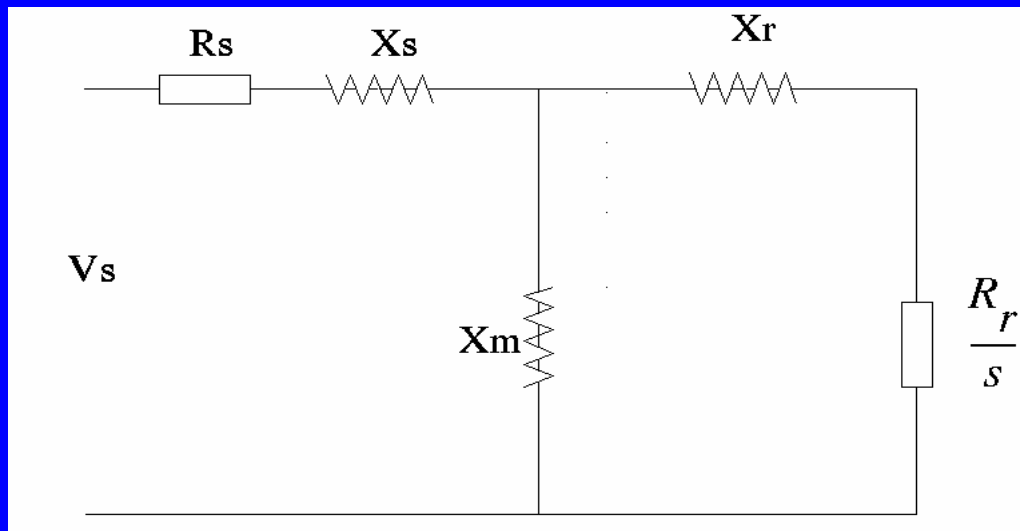


◆ Aggregate induction motor and static load

□ static load

$$P_d = P_0 \left(\frac{V}{V_0} \right)^\alpha, Q_d = Q_0 \left(\frac{V}{V_0} \right)^\beta$$

□ IM -- represent all down-stream compressor and other rotating load



$$\dot{s} = \frac{1}{2H} (T_m(s) - T_e(s, V))$$



Power System Model

$$\dot{x} = f(x, y, p)$$
$$0 = g(x, y, p)$$

◆ Dynamic variables	x_p, x_q, s	24
◆ Algebraic variables	P_d, Q_d	16
	V, \star	216
◆ Parameters		



Computation of Security Boundary

- ◆ Steady-state critical points in a loading direction (SNB, Hopf, ...)
- ◆ Security boundary
- ◆ Closest boundary points
- ◆ Security proximity index -- minimum distance



◆ System descriptions

$$\left. \begin{array}{l} \dot{x} = f(x, y, p) \\ 0 = g(x, y, p) \end{array} \right\} = F_G(x, y, p)$$

◆ Linearization

$$\Delta \dot{x} = J_s \cdot \Delta x$$

◆ Ray in parameter space

$$p = p_0 + \tau \cdot \gamma$$

$$\gamma = \sum_{i \in R^m} \beta_i e_i$$

$$\lambda = \alpha + j\omega$$



◆ General method for steady-state stability study

Minimize/maximize α^2

subject to:

$$\begin{aligned}F_G(x, y, +\tau\gamma) &= 0 \\J_s^T l' - a l' + w l'' &= 0 \\J_s^T l'' - a l'' - w l' &= 0 \\l^T l - 1 &= 0\end{aligned}$$



◆ Different characteristic points found by choice of stability constraints

α	ω	$\frac{d\alpha}{d\tau}$	Category
$\neq 0$	$\neq 0$	$= 0$	minimum or maximum damping pt
$= 0$	$\neq 0$	$\neq 0$	Hopf bifurcation point
$= 0$	$= 0$	≈ 0	SN bifurcation point



◆ Stability boundary

$$\begin{array}{l} SNB, \quad \sum_s \\ HB, \quad \sum_h \end{array}$$

◆ Closest bifurcation points

Minimize

$$\|\eta(p - p_0)\|$$

subject to

$$F(x, y, p) = 0$$

$$J_s^T l - j\omega l = 0$$

$$l^T l - 1 = 0$$



Application to NSW Grid

◆ Security boundary and closest point

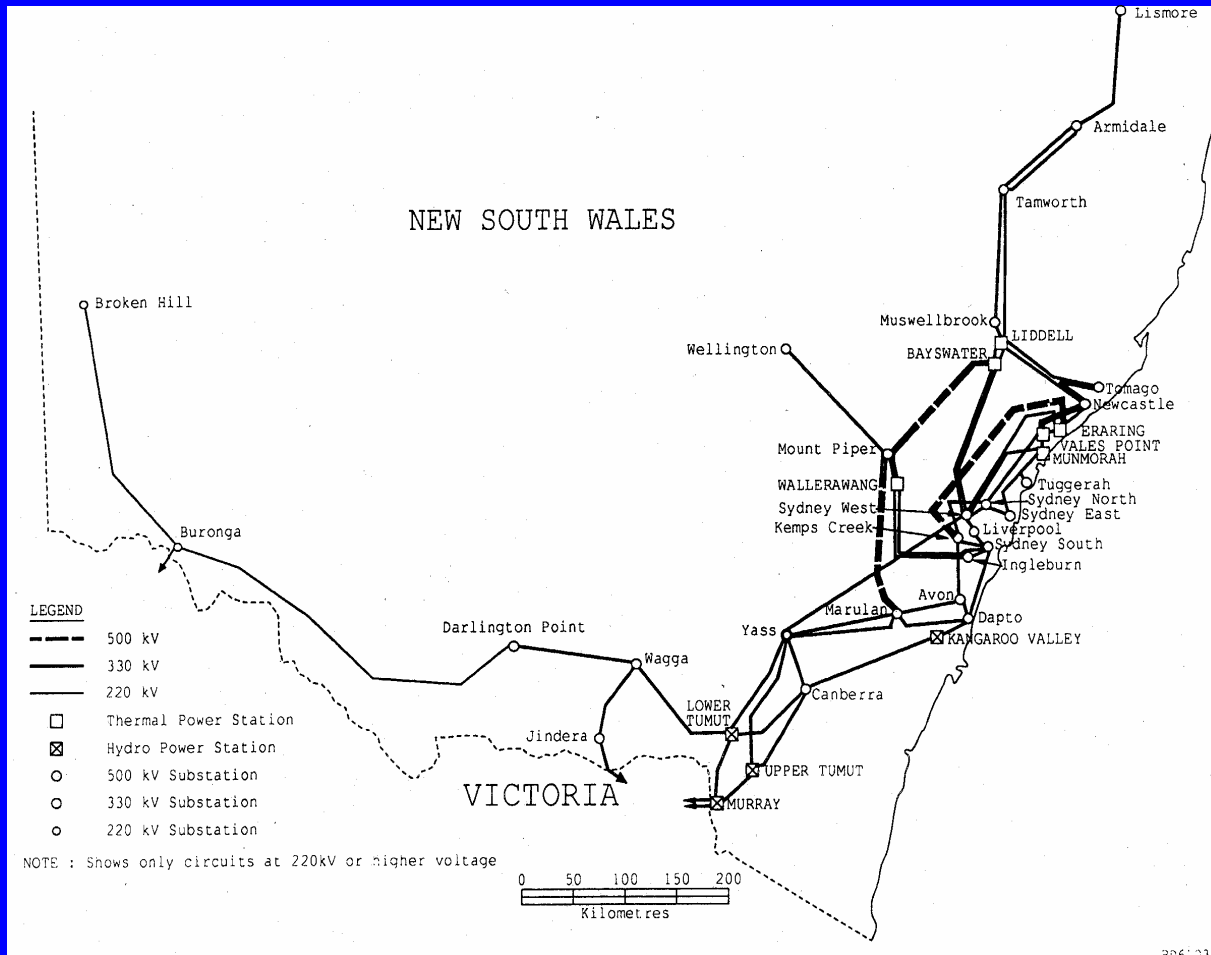
◆ Cases

□ All lines in service

□ Lines tripped out



◆ NSW System



Key load centres

Bus 74 (Newc 330)

Bus 76 (Tomago330)

Bus 3229 (Newc 132)

Bus 3207 (SydW 132)

Bus 3283 (Syd E 132)

Bus 3286 (Syd S 132)

Bus 3172 (Dapto 132)

Bus 3101 (Canb 132)



TABLE II Dynamic load parameters

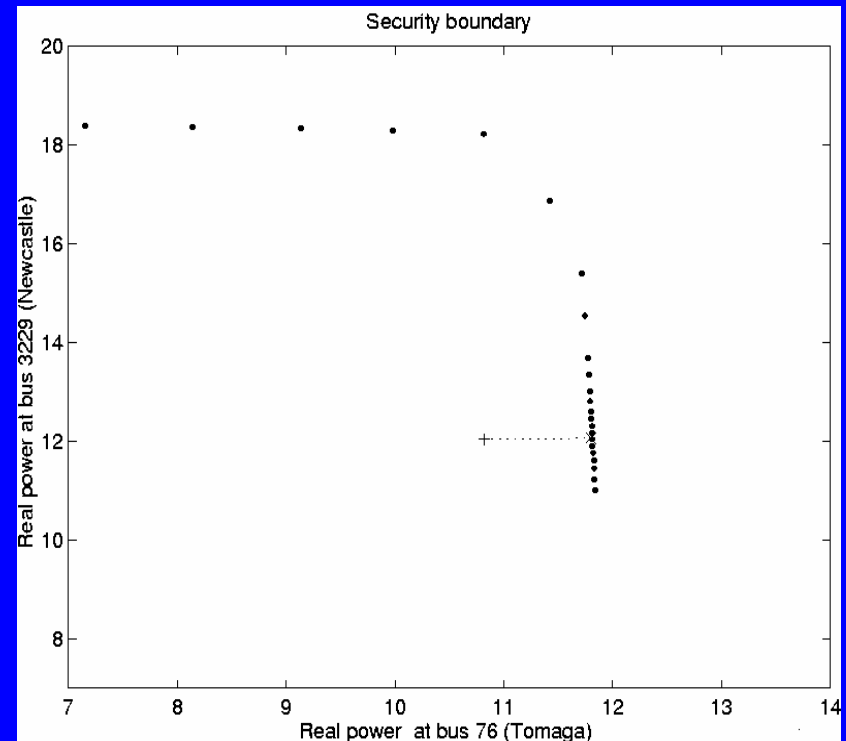
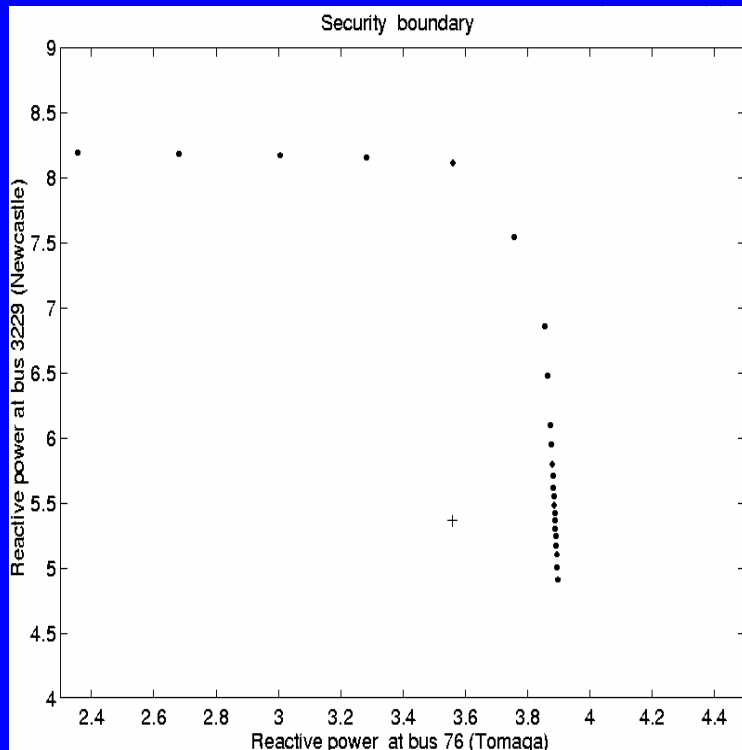
A-Tomago, B-Newcastle, C-Sydney West, D-Sydney east, E-Sydney South, F-Dapto, G-Canberra, H - Mbrk

Bus	Composi- tion	w_1 ,	w_2	w_3	α	β	IM set
A	Indus, Resi	35%	15%	50%	1	3	II
B	Indus, Resi	25%	15%	60%	1	3	II
C	Resi, Indus	30%	15%	55%	1	3	I
D	Resi, Com	60%	20%	20%	1	3	I
E	Resi, Com	85%	15%	0%	1	3	—
F	Resi	90%	10%	0%	1	3	—
G	Resi	85%	15%	0%	1	3	—
H	Indus, Resi	20%	10%	70 %	1	3	II



◆ Security boundary & closest point

□ Case 2 (a): after line 76-74 (Tomago-NewC) outage



Reactive power load, Q

Real power load, P

School of Electrical and Information Engineering
The University of Sydney

Closest point (1179.68Mw, 1206.17Mw)



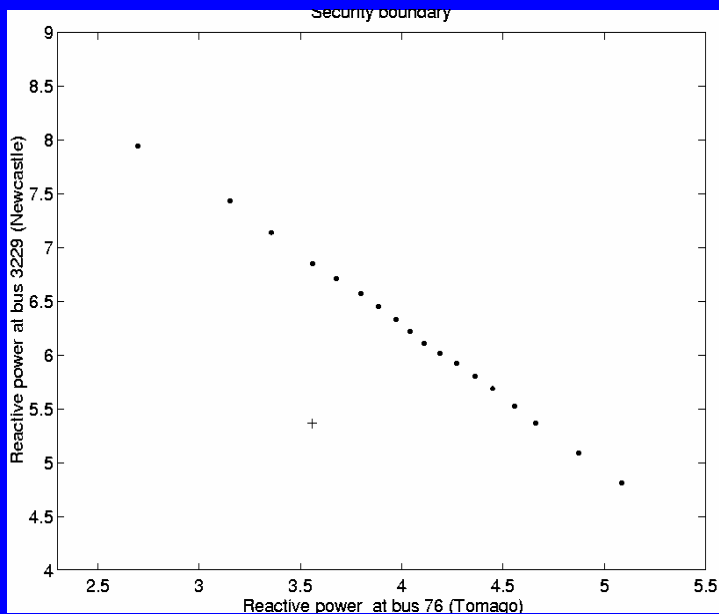
TABLE IV Case 2 Line76-74 Outage

Loading direction	Load Margin	Percentage Percentage
L_{76}	$113.6MW + j37.4Mvar$	10.5%
L_{3229}	$621.5MW + j276.9Mvar$	51.6%
both	$204.8MW + j79.9Mvar$	9.0%

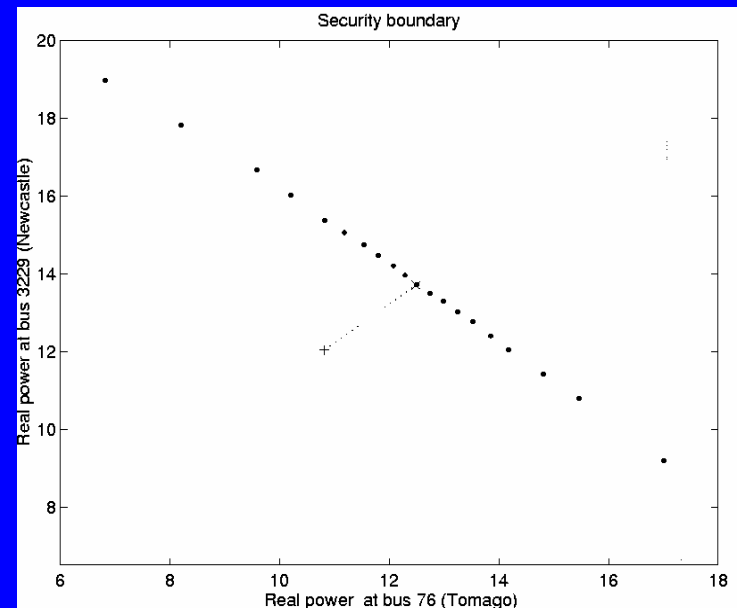


◆ Security boundary & closest point

□ Case 5 (b): after generation reduced at bus 201 (Liddell power station)



Reactive power load, Q



Real power load, P

Closest point (1249.24Mw, 1370.96Mw)



TABLE V Case 3-5, Load margins

	Load margin at buses 76 and 3229	percentage %
Case 3: line 86-76 out	841.5MW $+j328.5\text{Mvar}$	36.8%
Case 4: line 70-74 out	1275.7MW $+j498.1\text{Mvar}$	55.8%
Case 5: trip off gen 201	308.6MW $+j120.5\text{Mvar}$	13.5%



Impact of Load Modelling

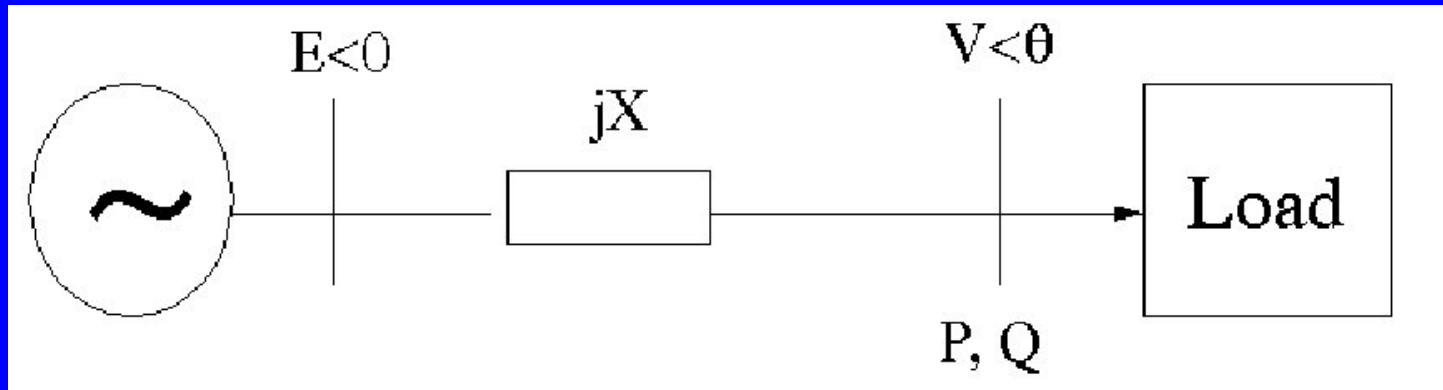
◆ Stability Margins

- Different load models
- Weighting factors
- Q_{limit} and tap regulation

◆ Dynamic Responses



Two Bus System



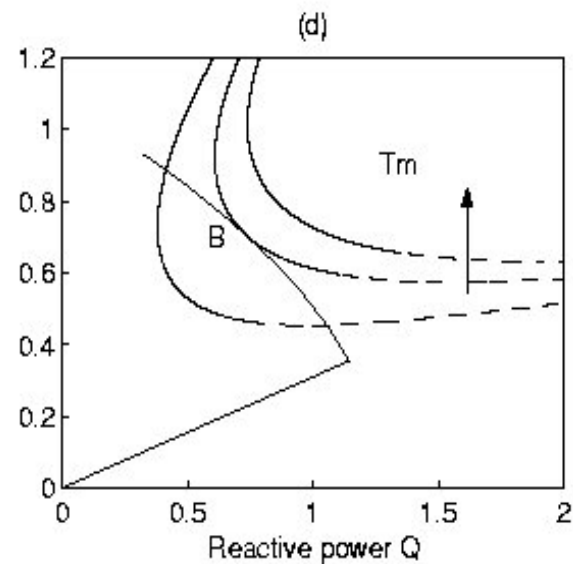
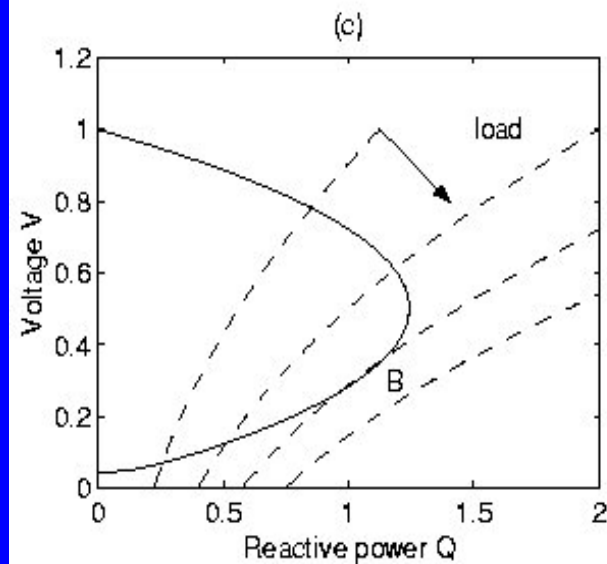
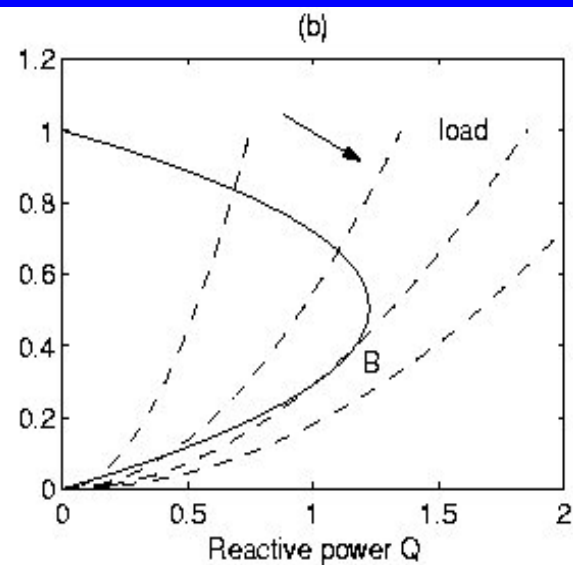
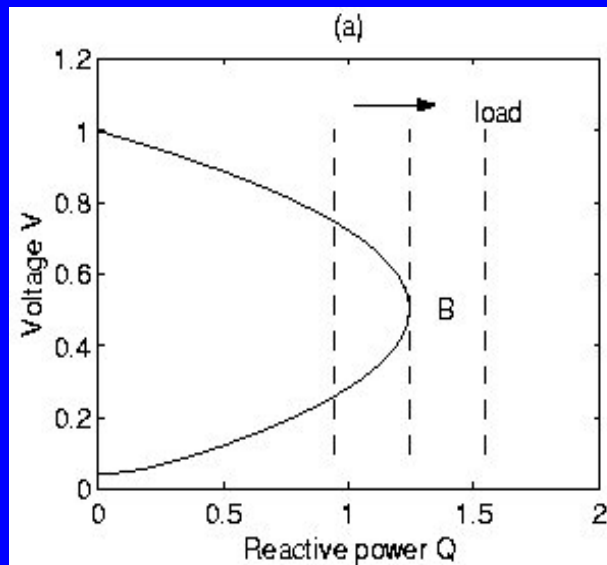


TABLE VI Margins with different load models

power	constant power load	exponential load ($\alpha, \beta = 0.5$)	composite dynamic load (Table II)
V_{cr} p.u.	0.7091	0.5377	0.7155
ΔL_{76}	70.9 MW + 23.3 Mvar	255.9 MW + 84.2 Mvar	113.6 MW + 37.4 Mvar
%	6.5%	23.6%	10.5%



TABLE VII Margins with different load parameters and weighting factors

	V_{cr}	margin at bus 76 MVA	percentage
$w_g = 0.7$	0.8241	$4.5 + j1.5$	0.4%
$w_g = 0.5$	0.7155	$113.6 + j37.4$	10.5%
$w_g = 0.1$	0.4212	$783.4 + j257.74$	72.4%
$\alpha_s = 0.8$ $\beta_s = 2$	0.5701	$232.4 + j76.47$	21.5%



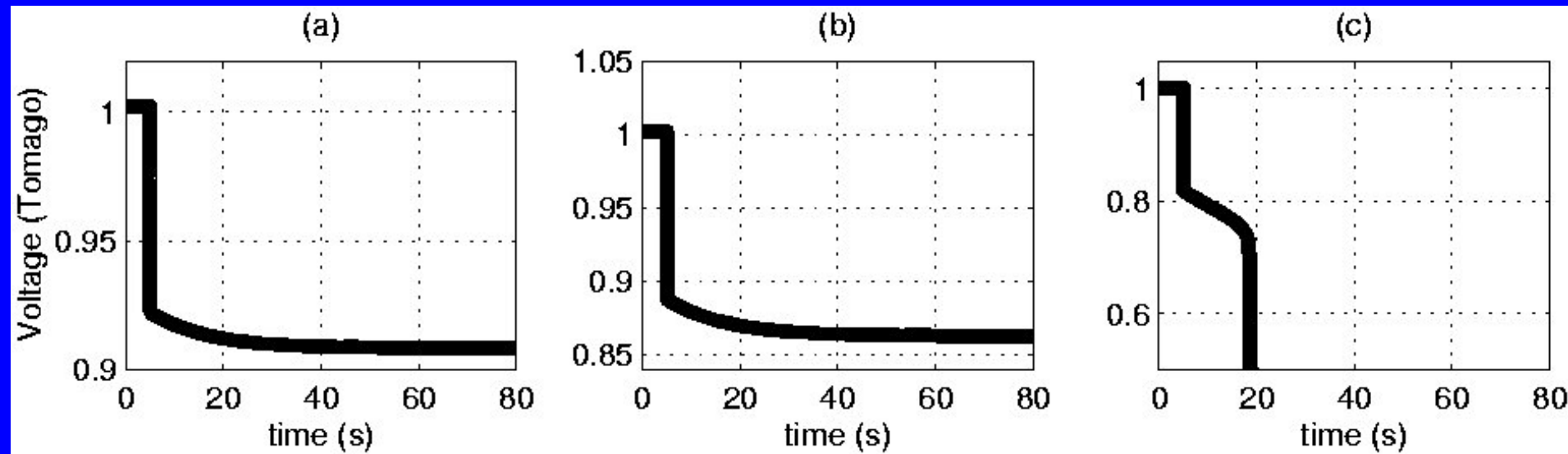
TABLE VIII Margins with/without Q_{limit} and tap regulation

	with	without
V_{cr} (pu)	0.7428	0.6905
ΔQ_{76}	60.46 MVAR	76.42 MVAR



Dynamic Response: Voltage at Tomago

a) Line fault; b) with 5% load increase after tripping; c) with 15% load increase



Coordinated control scheme

- ◆ Provide security enhancement

- ◆ Control actions

 - reactive power compensation, tap regulation, load control, FACTs, SVC, UPFC ...

- ◆ Traditionally, done one by one, trial and error



◆ Why coordination

- minimum overall effort / cost
- maximum control effect
- better voltage profile, hence better quality of supply

◆ Difficulty

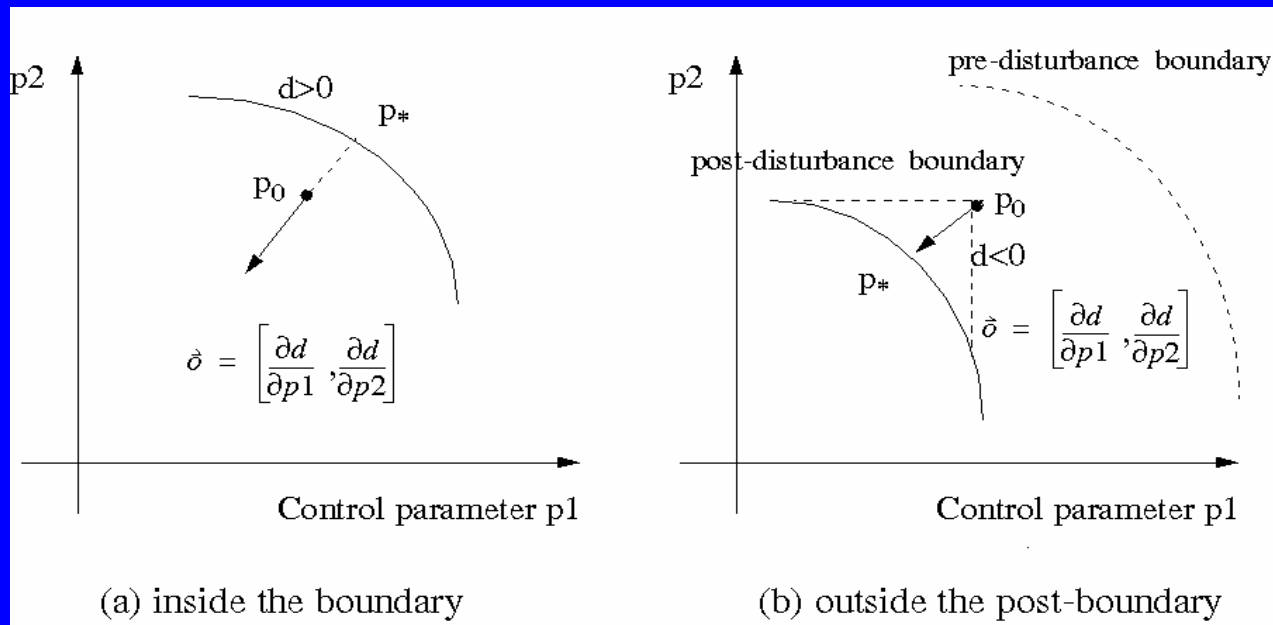
- Combination of dissimilar controls



◆ Optimal direction to increase security margin

□ sensitivity of minimum distance w.r.t. controls

$$\frac{\partial d}{\partial p} = \frac{-\omega f_p}{(\omega f_p) \left(\frac{p_* - p_0}{|p_* - p_0|} \right)}$$



◆ Illustrative example

□ Control parameters

--- Load (constant power factor) and capacitor at

Bus 76 (Tomago330)

Bus 3229 (Newc 330)

Bus 3207 (SydW 132)

Bus 3283 (Syd E 132)

Bus 3286 (Syd S 132)

--- taps at line

Bus 74 (Tomago330) to bus 3229 (Newc 330)

Bus 3207 (Syd W 132) to Bus 37 (Syd W 330)

Bus 42 (Syd E 330) to Bus 3283 (Syd E 132)

Bus 3286 (Syd S 132) to Bus 31 (Syd S 330)

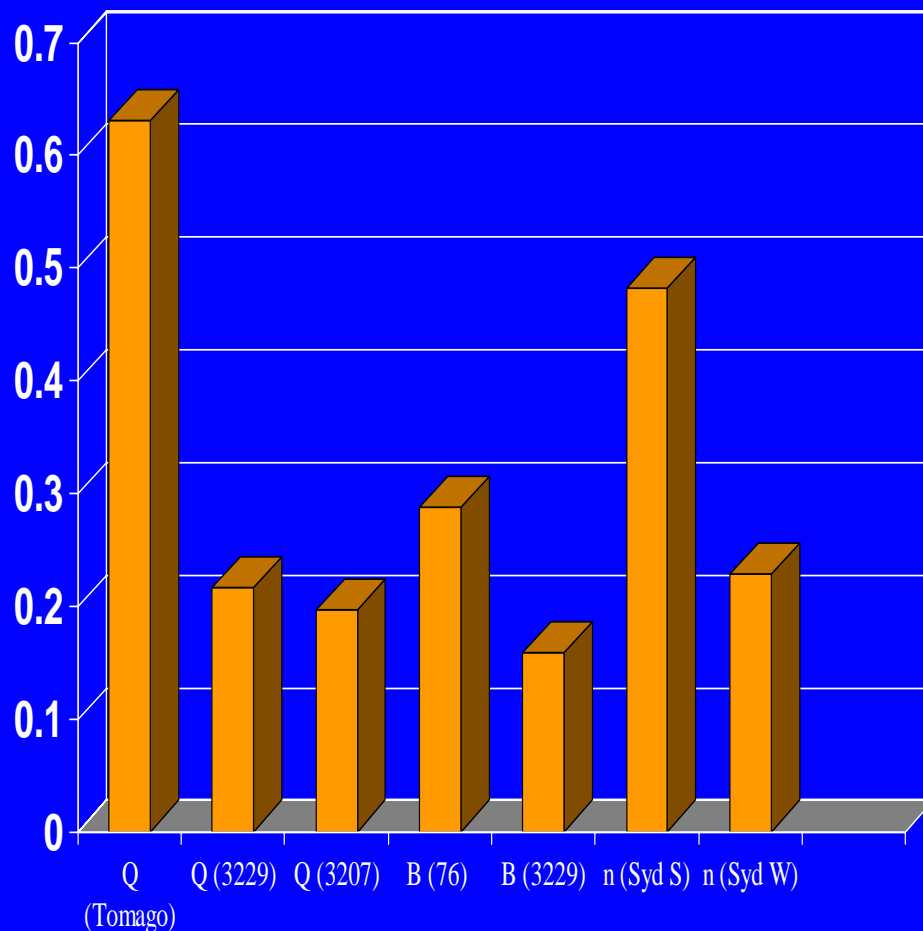
Bus 89 (Mbrk 330) to Bus 3271 (Mbrk 132)

□ minimum $d = +0.1530$ (with line 76-74 out of service and variation of all parameters)



□ Sensitivity of d w.r.t. controls

Controls	Sensitivity $\frac{\partial d}{\partial p}$
load 76 (Tomago)	-0.6306
load 3229 (Newcastle)	-0.2163
load 3207 (Sydney W)	-0.1969
load 3283 (Sydney E)	-0.1808
load 3286 (Sydney S)	-0.1335
capacitor 76 (Tomago)	0.2872
capacitor 3229 (Newcastle)	0.1580
capacitor 3207 (Sydney W)	0.1450
capacitor 3283 (Sydney E)	0.1335
capacitor 3286 (Sydney S)	0.1073
tap (74-3229)	0.0589
tap (3207-37)	0.1206
tap (42-3283)	0.2285
tap (3286-31)	-0.4826
tap (89-3271)	-0.0451



◆ Optimal scheduling of control actions

- Actual control sequence accounts for

 - combination of dissimilar controls

 - different response speeds

 - different dynamic characteristics

 - priority

- Optimal scheduling by

 - economic cost

 - availability of controls

- When, how to take actions at each step?



□ Problem formulation

$$\min \quad J(p) := \sum_{t=1}^N C(x_t, p_t), \quad p_t \in R^m, x_t \in R^m$$

subject to:

(i) controls capability constraints

$$p_t^{low} \leq p_t \leq p_t^{upper}, \quad t = 1, 2, \dots, N$$

(ii) stability constraints

$$S_{margin}(p_t) - S_{margin}(p_{t-1}) > \varepsilon$$



□ Dynamic programming (DP)

- stage-wise method

- backward recursive relationship

- disadvantage: curse of dimensionality

□ Differential dynamic programming (DDP)

- successive approximation

- computationally effective

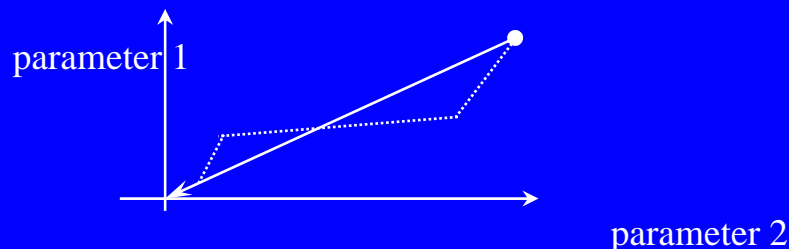


□ Numerical example

□ composite cost functions

-- economic cost, \$_{load} > \$_{cap} > \$_{tap}

-- minimum angle criterion



□ stages and system limits

Stages	Controls available
1	all capacitors
2	all capacitors, all taps
3	all capacitors, all taps, all loads

Controls	minimum	maximum
tap (74-3229)	0.857	1.048
tap (3207-37)	0.945	1.155
tap (42-3283)	0.857	1.048
tap (3286-31)	0.945	1.155
tap (89-3271)	0.857	1.048
capacitor 76 (Tomago)	0	190 Mvar
capacitor 3229 (Newcastle)	0	380 Mvar
capacitor 3207 (Sydney W)	0	500 Mvar
capacitor 3283 (Sydney E)	0	130 Mvar
capacitor 3286 (Sydney S)	0	300 Mvar
all loads	maximum shedding 50 Mw	



□ Optimal Scheduling ($\varepsilon=0.2$)

Control
actions

switch on **B=29.88 Mvar** at bus 76
switch on **B=24.49 Mvar** at bus 3229
switch on **B=21.40 Mvar** at bus 3207
switch on **B=21.47 Mvar** at bus 3283
switch on **B=12.46 Mvar** at bus 3286

move up tap 0.058 at tap 74-3229
move up tap 0.117 at tap 3207-37
move up tap 0.049 at tap 42-3283
move down tap 0.027 at 3286-31
move down tap 0.036 at 89-3271

switch on **B=24.58 Mvar** at bus 76
switch on **B=18.07 Mvar** at bus 3229
switch on **B=15.99 Mvar** at bus 3207
switch on **B=16.03 Mvar** at bus 3283
switch on **B= 9.91 Mvar** at bus 3286

shed load **16.95 Mw+j5.58Mvar** at 76
shed load **4.89 Mw +j 2.18 Mvar** at 3229
shed load **4.33 Mw + j1.01 Mvar** at 3207
shed load **3.86 Mw + j 0.88 Mvar** at 3283
shed load **2.48 Mw +j 0.17 Mvar** at 3286

move up tap 0.013 at tap 74-3229
move up tap 0.025 at tap 3207-37
move up tap 0.025 at tap 42-3283
move down tap 0.043 at 3286-31
move down tap 0.008 at 89-3271

switch on **B= 5.54 Mvar** at bus 76
switch on **B= 3.65 Mvar** at bus 3229
switch on **B= 3.26 Mvar** at bus 3207
switch on **B= 3.28 Mvar** at bus 3283
switch on **B= 2.17 Mvar** at bus 3286

1

2

3

Time axis
(stages)



Conclusions (Bologna)

- ◆ Quantify voltage stability margin
- ◆ Use composite load model
- ◆ General method for steady state voltage stability analysis
- ◆ Impact of load modelling
- ◆ Importance of accurate load representation
- ◆ Optimal control directions
- ◆ Co-ordination of dissimilar controls



◆Future Work

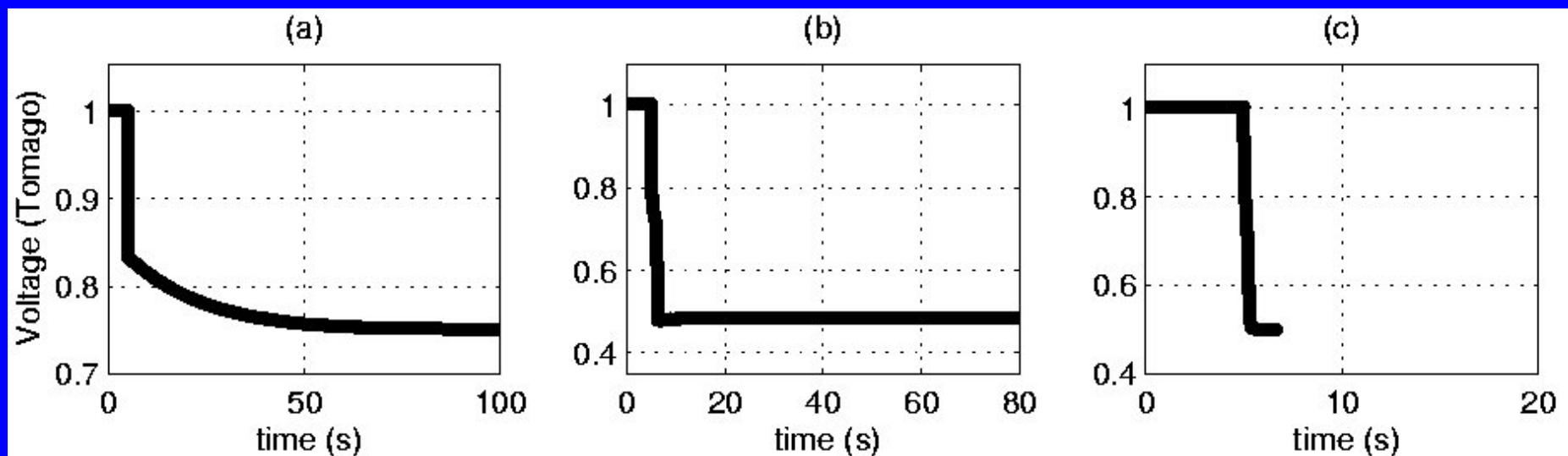
- More control devices (SVC, FACTS,UPFC...)
- Other objective functions (control times..)
- New search algorithm (Evolutionary algorithm...)
- Several disturbances
- Interrelationship of market structures with physical and practical implemented control
- Global control ideas



Extra Slides



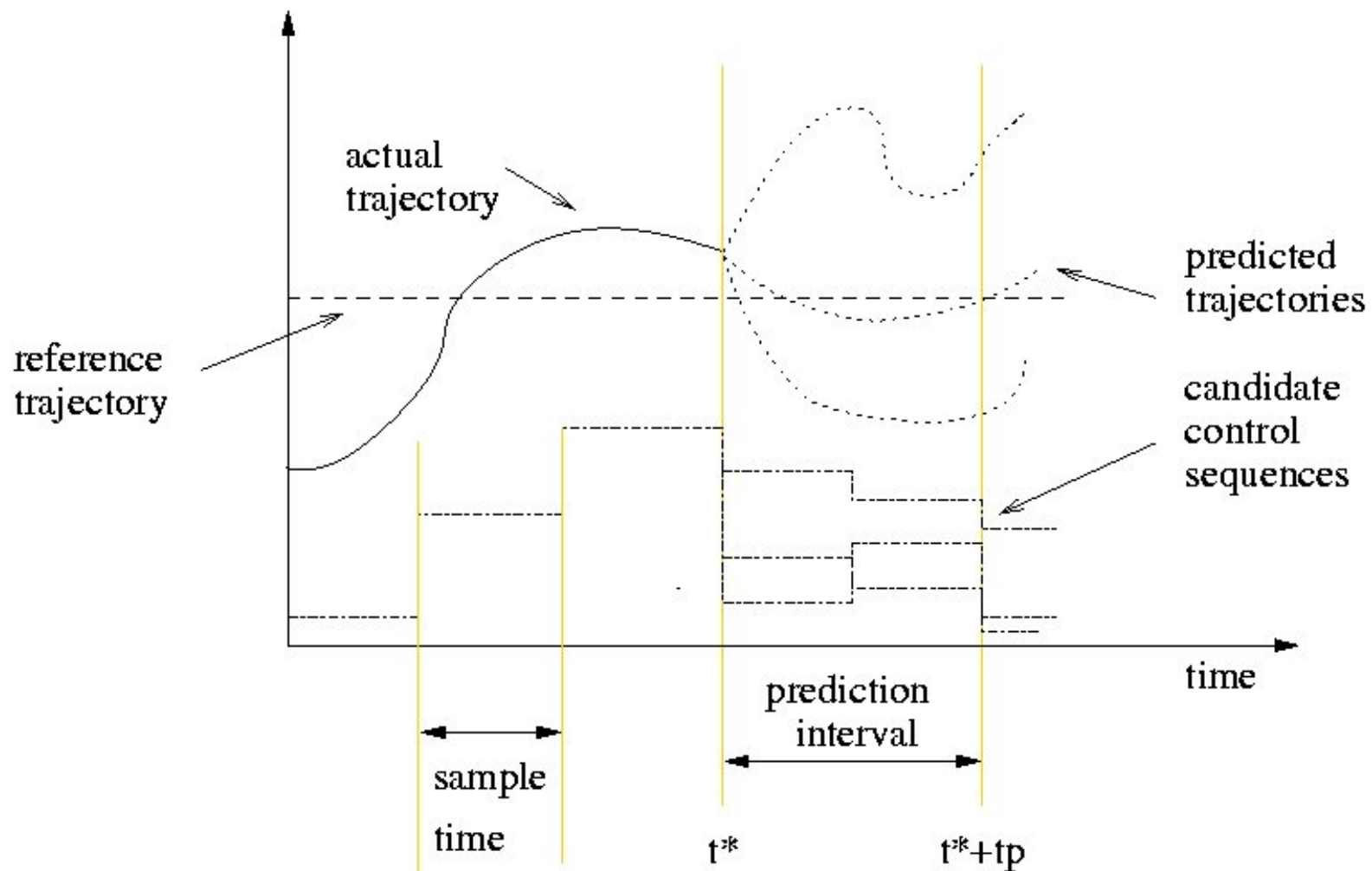
Dynamic Response: Voltage at Tomago
after line fault and 10% load increase; a)
 $\alpha_t=4, \beta_t=6$; b) $\alpha_t=1.5, \beta_t=1.5$; c) %IM (w_3)
increased 50% to 60%



Model Predictive Control Approach

- ◆ Widespread in process control
- ◆ Multivariable case comes naturally
- ◆ Constraint handling
- ◆ Future behaviour predicted for many candidate input sequences
- ◆ Optimal input sequence selected by (constrained) optimization





Optimization by Search

- ◆ All controls are switching actions
- ◆ Combinatorial optimization problem
- ◆ Organize control state space in tree structure
- ◆ Search tree for optimum
- ◆ Combinatorial explosion
- ◆ Search heuristics
- ◆ Similar problem as solved in chess computers!



Simulation Example

